



Article **Fractional-Order Multivariable Adaptive Control Based on a Nonlinear Scalar Update Law**

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Abstract: This paper proposes a new fractional-order model reference adaptive control (FOMRAC) framework for a fractional-order multivariable system with parameter uncertainty. The designed FOMRAC scheme depends on a fractional-order nonlinear scalar update law. Specifically, the scalar update law does not change as the input–output dimension changes. The main advantage of the proposed adaptive controller is that only one parameter online update is needed such that the computational burden in the existing FOMRAC can be relieved. Furthermore, we show that all signals in this adaptive scheme are bounded and the mean value of the squared norm of the error converges to zero. Two illustrative numerical examples are presented to demonstrate the efficiency of the proposed control scheme.

Keywords: fractional-order model reference adaptive control (FOMRAC); multivariable; fractionalorder nonlinear scalar update law; stability analysis

MSC: 26A33; 93C40



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1. Introduction

Over the past few decades, there have been considerable efforts towards linear systems with parameter uncertainty. Adaptive control has been one of the methods to solve this uncertainty. Among various adaptive control techniques, model reference adaptive control (MRAC) is the most popular and mature method, which provides feedback controller structures and adaptive laws for the control of systems to ensure that the closed-loop signals are bounded and the output or the state of the uncertain plant can asymptotically track the output or the state of the desired reference model, despite the uncertainties of the system parameters [1,2].

Fractional calculus has captured the attention of many scientists and engineers working in a variety of fields in recent years [3–7]. This is mostly owing to its ability to more accurately model specific physical systems than the traditional integer-order option, such as manipulator systems, multi-area power systems, multisource renewable energy systems, and electrical vehicles [8–12]. On the other hand, it is suitable for describing hereditary and memorial properties of various processes for which traditional integer-order differential equations fail to capture relevant phenomena, such as heat conduction and viscoelastic mechanics in materials with memory, and Zika virus transmission [13–18]. The expansion of MRAC to fractional-order systems, known as FOMRAC, has been proposed in the literature for more than a decade. Many useful results and applications for FOMRAC are studied based on a single-input single-output (SISO) plant. Among them, Shi et al. [19] proved the stability of the closed-loop control system strictly based on the continuous frequency distributed model. Then, a fractional-order composite MRAC was developed in [20] by incorporating the parameter estimate error into the parameter updating law to achieve better performance. Recently, the FOMRAC for multiple-input-multiple-output (MIMO) systems has been studied in the works of Norelys Aguila-Camacho and Manuel A. Duarte-Mermoud [21–24]. For example, in Ref. [21], they have proposed the standard fractional-order update laws and proved the Lyapunov stability of a fractional-order MIMO MRAC system by using a series of fractional inequalities. In Ref. [22], they further proved the convergence to zero of the mean value of the squared norm of the output error. In particular, the order of the plant and the adaptive laws in the above results are the same. In Ref. [24], they proposed the fractional-order update laws whose order is smaller than that of the plant. However, the above results usually require online estimation of multiple unknown parameters, and as the input–output dimension of the FOMRAC system increases, the number of parameters that need to be updated online also increases, which greatly increases the computational burden and limits the practicality of FOMRAC. Therefore, the issue of how to reduce the number of parameters estimated online is a critical problem to be solved for the MIMO FOMRAC system.

In this article, a new FOMRAC framework is proposed for fractional-order multivariable systems with parameter uncertainty. The proposed fractional-order adaptive controller with state feedback depends on a fractional-order nonlinear scalar update law. Specifically, the scalar update law does not change as the input–output dimension changes. The major contributions of this paper can be formulated as follows:

- 1. we design a new FOMRAC scheme to handle the parameter uncertainty and to ensure the system error stability and closed-loop signal boundedness;
- 2. using the proposed FOMRAC framework, only one parameter online update is needed such that the control scheme is computationally inexpensive;
- 3. we conduct a complete theoretical analysis of the boundedness of all signals involved in this adaptive scheme and the convergence to zero of the mean value of the squared norm of the system error for the proposed control architecture;
- 4. we verify the effectiveness of this control design by two illustrative numerical examples.

This paper is organized as follows. Section 2 briefly gives some basic concepts about fractional calculus and some necessary lemmas. Section 3 presents the FOMRAC problem. The adaptive controller based on a fractional-order scalar update law and the stability analysis for the adaptive control architecture are shown in the main results given in Section 4. Section 5 presents two numerical examples to clarify the validity of the proposed approach. Section 6 contains the conclusions and future works.

2. Preliminaries

This section introduces some fundamental concepts of fractional calculus, as well as some properties of fractional operators that will be used throughout the paper.

Notation. The following notations are used throughout the whole paper. Let *R* and R^+ denote the set of real, non-negative real numbers, respectively. R^n denotes the set of $n \times 1$ real column vectors, $R^{n \times m}$ denotes the set of $n \times m$ real matrices. The matrix *P* is symmetric if $P = P^T$. P > 0 denotes the positive definite matrix *P*. tr(A) denotes the trace of the matrix *A*.

Definition 1. *Riemann–Liouville fractional integral* [3].

$$_{t_0}I_t^{\beta}g(t) = \frac{1}{\Gamma(\beta)} \int_{t_0}^t \frac{g(\tau)}{(t-\tau)^{1-\beta}} d\tau, \quad t > t_0, \ \beta > 0,$$
(1)

where $\Gamma(\beta)$ is the Gamma function.

Definition 2. Caputo Fractional Derivative [3].

$${}_{t_0}^{C} D_t^{\beta} g(t) = \frac{1}{\Gamma(n-\beta)} \int_{t_0}^t \frac{g^n(\tau)}{(t-\tau)^{\beta-n+1}} d\tau, \quad t > t_0,$$
(2)

with $n - 1 < \beta < n, \beta > 0$.

The following lemmas will be used to prove the main results in this paper.

Lemma 1 ([23]). Let $g(t) \in \mathbb{R}^n$ be a vector of differentiable functions. Then, for all $t > t_0$, the following relationship holds

$${}_{t_0}^C D_t^\beta [g^T(t) Pg(t)] \le 2g^T(t) P_{t_0}^C D_t^\beta g(t),$$
(3)

where $\beta \in (0, 1]$, and $P \in \mathbb{R}^{n \times n}$, satisfying $P = P^T > 0$.

Lemma 2 ([23]). Let $A(t) \in \mathbb{R}^{m \times n}$ be a time-varying differentiable matrix. Then, for any time instant $t \ge t_0$, the following relationship holds

Lemma 3 ([22]). Let $g(.) : R^+ \to R$ be a bounded nonnegative function. If there exists some $\beta \in (0, 1]$ such that

$$\frac{1}{\Gamma(\beta)} \int_{t_0}^t \frac{g(\tau)}{(t-\tau)^{1-\beta}} d\tau < L, \quad \forall t > t_0, with \ L \in (0,\infty),$$
(5)

then

$$\lim_{t \to \infty} t^{\beta - \varepsilon} \frac{\int_{t_0}^t g(\tau) d\tau}{t} = 0, \quad \forall \varepsilon > 0.$$
(6)

3. FOMRAC Problem

Consider a fractional-order MIMO plant with parameter uncertainty given by

$$C_{t_0}^C D_t^B x_p(t) = A_p x_p(t) + B_p u(t),$$

$$x_p(t_0) = x_{p0}, \quad t \ge t_0,$$
(7)

where $x_p(t) \in \mathbb{R}^n$ is a measurable state vector, $u(t) \in \mathbb{R}^m$ is the control input and the fractional order $\beta \in (0, 1]$. In addition, $A_p \in \mathbb{R}^{n \times n}$ is an unknown constant state matrix capturing the parameter uncertainty in the fractional-order MIMO plant, and $B_p \in \mathbb{R}^{n \times m}$ denotes a known control matrix. For the well-posedness of the FOMRAC problem, we assume that the pair (A_p, B_p) is controllable. Recall that the controllability conditions ensure that the control input u(t) has sufficient access to the internal state to stabilize all unstable modes of a plant.

In addition, the fractional-order reference model is chosen by

$${}_{t_0}^C D_t^\beta x_m(t) = A_m x_m(t) + B_m r(t), \quad x_m(t_0) = x_{m0}, \quad t \ge t_0,$$
(8)

where $x_m(t) \in \mathbb{R}^n$ is a reference state vector, $A_m \in \mathbb{R}^{n \times n}$ is Hurwitz and known, $B_m \in \mathbb{R}^{n \times m}$ is known and $r(t) \in \mathbb{R}^m$ is bounded and piecewise continuous. It is assumed that $x_m(t)$, for all $t \ge t_0$, represents the desired trajectory for $x_p(t)$.

The objective of the FOMRAC is to design a feedback controller u(t) such that all the signals remain bounded and, ideally, the state of the uncertain system $x_p(t)$ can track the state of the reference model $x_m(t)$ asymptotically.

Next, define an ideal feedback controller that perfectly eliminates the uncertainty and allows $x_p(t)$ to follow $x_m(t)$ as

$$u^{*}(t) = Kr(t) + \Theta^{*}x_{p}(t), \quad t \ge t_{0}.$$
(9)

Here, $K \in \mathbb{R}^{m \times m}$, $\Theta^* \in \mathbb{R}^{m \times n}$ are the ideal control gains chosen such that the matching conditions

$$A_m = A_p + B_p \Theta^*, \tag{10}$$

and

$$B_m = B_p K, \tag{11}$$

hold. Since B_p is known, K can be obtained directly from the matching condition (11). Since A_p is unknown, Θ^* is also unknown.

The actual adaptive controller is an estimate of the ideal controller, with the purpose of approaching the ideal controller in the limit. Let

$$u(t) = Kr(t) + \Theta(t)x_p(t), \quad t \ge t_0,$$
(12)

be the actual adaptive controller, where $\Theta(t) : \mathbb{R}^+ \to \mathbb{R}^{m \times n}$ is the estimate of Θ^* .

Now, define the estimation error as $\hat{\Theta}(t) = \Theta(t) - \Theta^*$. Then, the closed-loop plant model can be written as

$${}_{t_0}^C D_t^P x_p(t) = A_m x_p(t) + B_m r(t) + B_p \tilde{\Theta}(t) x_p(t), \quad x_p(t_0) = x_{p0}, \quad t \ge t_0.$$
(13)

Let $e(t) = x_p(t) - x_m(t)$ be the tracking error. Then, the tracking error equation is expressed as

$${}_{t_0}^C D_t^{\beta} e(t) = A_m e(t) + B_p \tilde{\Theta}(t) x_p(t), \quad e(t_0) = e_0, \quad t \ge t_0.$$
(14)

The goal of FOMRAC is changed to design the adaptive laws to adjust $\Theta(t)$ in such a way that all the closed-loop signals remain bounded and ideally $\lim ||e(t)|| = 0$.

In 2015, Duarte-Mermoud, M. A. et al. [23] designed the standard fractional-order update laws

$$\begin{aligned} & {}^C_{t_0} D^B_t \Theta(t) = -B^T_p Pe(t) x^T_p(t), \\ & \Theta(t_0) = \Theta_0, \quad t \ge t_0, \end{aligned}$$

$$(15)$$

where $P \in \mathbb{R}^{n \times n}$ is a positive definite symmetric matrix satisfying the Lyapunov equation

$$A_m^T P + P A_m = -Q, (16)$$

where $Q \in \mathbb{R}^{n \times n}$ is positive definite. Since A_m is a Hurwitz constant matrix, it follows from converse Lyapunov theory [25,26] that, for any given matrix Q > 0, there exists a unique matrix P > 0 that satisfies the Lyapunov Equation (16). Recently, Aguila-Camacho, N. et al. [24] designed the fractional-order update laws for $\Theta(t)$ as

$$\begin{aligned} {}^{C}_{t_0} D^{\alpha}_t \Theta(t) &= -B^T_p Pe(t) x^T_p(t), \\ \Theta(t_0) &= \Theta_0, \quad t \ge t_0, \end{aligned}$$

$$(17)$$

where $0 < \alpha < \beta \leq 1$. This denotes that the order of the adaptive laws can be smaller than the order of the plant. Specifically, when the plant under control is of integer order, the adaptive laws can be fractional, which is one of the most promising applications from the practical point of view.

In the above works, $\Theta(t) \in \mathbb{R}^{m \times n}$ is an adaption parameter matrix satisfying $m \times n$ update laws, where m and n are the dimension of the input and output, respectively. However, as the input–output dimension of the FOMRAC system increases, the number of parameters that need to be updated online also increases, which greatly increases the computational burden of the online part and limits the practicality of FOMRAC. Therefore, how to reduce the number of parameters estimated online is a critical problem to be solved for the MIMO FOMRAC system.

4. Main Results

Following the analysis above, we aim to explore an adaptive control architecture aiming at mitigating the the number of parameters to be updated online in FOMRAC. To achieve this, we design the fractional-order scalar function $\varphi(t) \in R$. Then, ${}_{t_0}^C D_t^\beta \Theta(t) = \delta^T {}_{t_0}^C D_t^\beta \varphi(t)$, where $\delta = (\delta_{i,j}) \in R^{n \times m}$ is a designed non-zero parameter matrix. Now, in order to determine the scalar update law for FOMRAC, let the estimation error have the form provided by $\tilde{\Theta}(t) = \delta^T \varphi(t)$. The equations of the plant model and the tracking error can thus be written as

$${}_{t_0}^{C} D_t^{\beta} x_p(t) = A_m x_p(t) + B_m r(t) + B_p \delta^T \varphi(t) x_p(t),$$
(18)

and

$${}_{t_0}^C D_t^\beta e(t) = A_m e(t) + B_p \delta^T \varphi(t) x_p(t), \quad e(t_0) = e_0, \quad t \ge t_0,$$
(19)

respectively.

The main finding of this research is stated in the following theorem.

Theorem 1. Consider the uncertain fractional-order multivariable system described by (7), the reference model given by (8) and the feedback controller given by (12). If the parameter update laws are constructed as

$${}^{C}_{t_0} D^{\beta}_t \Theta(t) = \delta^{T}{}^{C}_{t_0} D^{\beta}_t \varphi(t)$$
⁽²⁰⁾

with the scalar update law

$${}_{t_0}^C D_t^\beta \varphi(t) = -\frac{1}{tr(\delta\delta^T)} e^T(t) P B_p \delta^T x_p(t), \quad \varphi(t_0) = \varphi_0, \tag{21}$$

where $e(t) = x_p(t) - x_m(t)$ is the the tracking error, and $P \in \mathbb{R}^{n \times n}$ is a positive-definite solution of the Lyapunov Equation (16), then it holds that:

- (*i*) The tracking error e(t), the scalar function $\varphi(t)$, the system state $x_p(t)$, the estimation error $\tilde{\Theta}(t)$ and parameter $\Theta(t)$ remain bounded for all $t \ge t_0$;
- (ii) The mean value of $||e(t)||^2$ converges to zero when $t \to \infty$.

Proof. Consider the quadratic Lyapunov function given by

$$V(e(t),\varphi(t)) = e^{T}(t)Pe(t) + tr\{[\delta^{T}\varphi(t)]^{T}[\delta^{T}\varphi(t)]\},$$
(22)

where $P = P^T > 0$ satisfies (16), and note that V(0,0) = 0. Since P > 0, $V(e(t), \varphi(t)) > 0$ for all $(e(t), \varphi(t)) \neq (0, 0)$.

According to Lemmas 1 and 2, we can obtain the β -order Caputo derivative of $V(e(t), \varphi(t))$ as follows:

$${}_{t_0}^{C} D_t^{\beta} V(e(t), \varphi(t)) \le 2e^T(t) P_{t_0}^{C} D_t^{\beta} e(t) + tr\{[\delta^T \varphi(t)]_{t_0}^{TC} D_t^{\beta}[\delta^T \varphi(t)]\}.$$
(23)

Now, substituting (19) and (16) into (23), we can obtain that

$$\begin{aligned} & \stackrel{C}{}_{t_0} D_t^{\beta} V(e(t), \varphi(t)) \\ & \leq -e^T(t) Q e(t) + 2e^T(t) P B_p \delta^T \varphi(t) x_p(t) \\ & + 2tr(\delta \delta^T) \varphi(t)_{t_0}^C D_t^{\beta} \varphi(t). \end{aligned}$$
(24)

If the scalar update law is designed as (21), then we can infer that

$${}_{t_0}^{C} D_t^{\beta} V(e(t), \varphi(t)) \le -e^T(t) Q e(t).$$
(25)

Accordingly,

$${}_{t_0}^C D_t^\beta V(e(t), \varphi(t)) \le -\lambda_{\min}(Q) \|e(t)\|^2 \le 0.$$
(26)

Applying the fractional integral of order β to inequality (26), we can obtain that

$$e^{T}(t)Pe(t) + tr\{[\delta^{T}\varphi(t)]^{T}\delta^{T}\varphi(t)\} - e^{T}(t_{0})Pe(t_{0}) - tr\{[\delta^{T}\varphi(t_{0})]^{T}\delta^{T}\varphi(t_{0})\}.$$

$$\leq -\lambda_{min}(Q)_{t_{0}}I_{t}^{\beta}\|e(t)\|^{2}.$$
(27)

Since
$$\lambda_{min}(Q)_{t_0} I_t^{\beta} \|e(t)\|^2 \ge 0, \forall \ge t_0$$
, then
 $e^T(t) Pe(t) + tr\{[\delta^T \varphi(t)]^T \delta^T \varphi(t)\} \le e^T(t_0) Pe(t_0) + tr\{[\delta^T \varphi(t_0)]^T \delta^T \varphi(t_0)\}.$ (28)

Considering the boundedness of initial values for $e(t_0)$, $\varphi(t_0)$, then inequality (28) implies that e(t) and $\varphi(t)$ remain bounded for all $t \ge t_0$. Since $x_p(t) = x_m(t) + e(t)$, $\tilde{\Theta}(t) = \delta^T \varphi(t)$ and the boundedness of $x_m(t)$, then system state $x_p(t)$ and estimation error $\tilde{\Theta}(t)$ are bounded for all $t \ge t_0$. Accordingly, parameter $\Theta(t)$ is bounded for all $t \ge t_0$.

Since e(t) and $\varphi(t)$ are bounded, then it can be obtained that ${}_{t_0}I_t^{\beta} || e(t) ||^2 \le \infty$. Then, using Lemma 3, we can conclude that

$$\lim_{t \to \infty} t^{\beta - \varepsilon} \frac{\int_{t_0}^t \|e(\tau)\|^2 d\tau}{t} = 0, \quad \forall \varepsilon > 0.$$
⁽²⁹⁾

Accordingly, the mean value of $||e(t)||^2$ converges to zero when $t \to \infty$, and this completes the proof. \Box

A block diagram showing the adaptive control framework based on the fractionalorder scalar update law is given in Figure 1.





5. Simulation Example

In this section, we present two numerical examples to demonstrate the utility of the proposed adaptive control scheme. The scheme was implemented in Matlab/Simulink, using the FOMCON Toolbox to obtain the required results.

Example 1. Let us consider a MIMO fractional-order linear time-invariant plant with parameter uncertainty, which is given by

$$C_{0}D_{t}^{\beta}x_{p}(t) = A_{p}x_{p}(t) + \begin{bmatrix} 0.8 & 0.8 \\ 0 & 0.8 \end{bmatrix} u(t),$$

$$x_{p}(0) = \begin{bmatrix} 0.06 \\ 0.06 \end{bmatrix}, \quad t \ge 0,$$

$$(30)$$

where $x_p(t) = [x_{p_1}(t), x_{p_2}(t)]^T$. Here, A_p is an unknown constant state matrix that denotes the parameter uncertainty. For simulation purposes, the true $A_p = \begin{bmatrix} 1 & 1 \\ -1 & -1 \end{bmatrix}$.

For this study, we choose the reference model given by

$$\begin{split} {}_{0}^{C}D_{t}^{\beta}x_{m}(t) &= \begin{bmatrix} 0 & 1 \\ -4 & -2 \end{bmatrix} x_{m}(t) + \begin{bmatrix} 0 & 1 \\ 4 & 1 \end{bmatrix} r(t), \\ x_{m}(0) &= \begin{bmatrix} 0.1 \\ 0.1 \end{bmatrix}, \quad t \geq 0, \end{split}$$

where $x_m(t) = [x_{m_1}(t), x_{m_2}(t)]^T$. Consequently, the ideal control gains become $K = \begin{bmatrix} -5 & 0 \\ 5 & 1.25 \end{bmatrix}$ and $\Theta^* = \begin{bmatrix} 2.5 & 1.25 \\ -3.75 & -1.25 \end{bmatrix}$.

For this case, matrices $Q = I_{2\times 2}$ and $P = \begin{bmatrix} \frac{2}{3} & \frac{1}{8} \\ \frac{1}{8} & \frac{5}{16} \end{bmatrix}$ exist such that $A_m^T P + PA_m = -Q$. Further, we choose $\delta = \begin{bmatrix} 0 & 3 \\ -5 & -5 \end{bmatrix}$ for the proposed fractional-order nonlinear scalar update law given by (21). Then, the update law of $\Theta(t)$ is

$${}_{0}^{C}D_{t}^{\beta}\Theta(t) = \delta^{T}{}_{0}^{C}D_{t}^{\beta}\varphi(t),$$

where

$${}_{0}^{C}D_{t}^{\beta}\varphi(t) = \frac{1}{59}[(-3.9e_{1}(t) - 1.05e_{2}(t))x_{p_{1}}(t) + (12.5e_{1}(t) + 2.25e_{2}(t))x_{p_{2}}(t)].$$

For convenience, the reference signal r(t) is chosen as the unit step signal and the fractional order used is $\beta = 0.8$. Then, we have the following numerical results displayed in Figures 2–6.



Figure 2. Time evolution of tracking error $e_1(t)$.



Figure 3. Time evolution of tracking error $e_2(t)$.



Figure 4. Plant and model reference outputs $x_{p_1}(t)$ and $x_{m_1}(t)$.



Figure 5. Plant and model reference outputs $x_{p_2}(t)$ and $x_{m_2}(t)$.



Figure 6. Scalar function $\varphi(t)$.

Figures 2–6 show that, as stated by the analysis above, the tracking error, the scalar function $\varphi(t)$ and the system state remain bounded for every $t \ge 0$. In addition to the boundedness of the closed-loop signals, Figures 2 and 3 show that the tracking error converges to zero, although only the convergence of the mean value of $||e(t)||^2$ was analytically proven.

External Disturbance

To illustrate the robustness of the system, we consider that the system (30) is subject to a parametric variation of the state matrix A_p in the form $A_{newp} = A_p + \epsilon D$ at t = 20 s, where $\epsilon > 0$ and $D \in \mathbb{R}^{n \times n}$. Here, we choose $\epsilon = 0.001$, $D = \begin{bmatrix} 1 & 1 \\ 1 & 1 \end{bmatrix}$, and the simulation results are shown in Figures 7 and 8. This example shows that, even in the case of an external

disturbance to the system (30), the proposed FOMRAC scheme maintains its performance and the tracking of the reference model trajectory.



Figure 7. System response of e_1 under the external disturbances.



Figure 8. System response of *e*² under the external disturbances.

Example 2. Let us consider a fractional-order multivariable system with parameter uncertainty, where $x_p(t) = [x_{p_1}(t), x_{p_2}(t)]^T$, A_p is unknown, and B_p is known and given by $B_p = [1, 1]^T$, $A_m = \begin{bmatrix} -1 & 0 \\ 0 & -2 \end{bmatrix}$, $B_m = [1, 1]^T$. For the purpose of simulation, the true $A_p = \begin{bmatrix} -4 & 1 \\ -3 & -1 \end{bmatrix}$. Therefore, the ideal control gain becomes K = 1 and $\Theta^* = [3, -1]$.

In the simulation, we set matrix $P = I_{2\times 2}$ and $Q = \begin{bmatrix} 2 & 0 \\ 0 & 4 \end{bmatrix}$ exist such that $A_m^T P + PA_m = -Q$.

From (15), (17) and (21), we can obtain that

$$\int_{0}^{B} \Theta(t) = \left[-(e_{1}(t) + e_{2}(t))x_{p_{1}}(t), -(e_{1}(t) + e_{2}(t))x_{p_{2}}(t) \right],$$

$$\int_{0}^{C} D_{t}^{\alpha} \Theta(t) = \left[-(e_{1}(t) + e_{2}(t))x_{p_{1}}(t), -(e_{1}(t) + e_{2}(t))x_{p_{2}}(t) \right],$$

$${}_0^C D_t^\beta \varphi(t) = -\frac{1}{tr(\delta\delta^T)} (e_1(t) + e_2(t)) \delta^T x_p(t),$$

where $0 < \alpha < \beta \leq 1$, and the number of update laws in the standard fractional-order adaptive controller and the fractional adaptive controller in [24] is 2, and ours is only 1. Therefore, compared with the other two adaptive controllers, our controller can reduce the number of parameters updated online.

To further demonstrate the efficacy of the proposed adaptive control architecture, we compare the evolution of system state and system error with the standard fractional-order adaptive controller in [23], the fractional adaptive controller in [24] and our proposed adaptive controller. The initial values correspond to $x_p(0) = [0.1, 1]^T$, $x_m(0) = [1, 2]^T$, the fractional order used is $\beta = 0.8$, and the reference signal r(t) = 15sin(8t) + 10cos(6t). For convenience, we choose $\alpha = 0.6$ for the fractional adaptive controller in [24], and $\delta = [-1, 1]^T$ for our proposed adaptive controller. Then, we have the following numerical results shown in Figures 9–12.



Figure 9. Time evolution of tracking error $e_1(t)$ with the standard fractional order adaptive controller in Duarte-Mermoud, M. A. et al. [23], the fractional adaptive controller in Aguila-Camacho, N. et al. [24], and our proposed adaptive controller with the fractional-order scalar update law in this paper.



Figure 10. Time evolution of tracking error $e_2(t)$ with the standard fractional order adaptive controller in Duarte-Mermoud, M. A. et al. [23], the fractional adaptive controller in Aguila-Camacho, N. et al. [24], and our proposed adaptive controller with the fractional-order scalar update law in this paper.



Figure 11. Plant and model reference outputs $x_{p_1}(t)$ and $x_{m_1}(t)$ with the standard fractional order adaptive controller in Duarte-Mermoud, M. A. et al. [23], the fractional adaptive controller in Aguila-Camacho, N. et al. [24], and our proposed adaptive controller with the fractional-order scalar update law in this paper.



Figure 12. Plant and model reference outputs $x_{p_2}(t)$ and $x_{m_2}(t)$ with the standard fractional order adaptive controller in Duarte-Mermoud, M. A. et al. [23], the fractional adaptive controller in Aguila-Camacho, N. et al. [24], and our proposed adaptive controller with the fractional-order scalar update law in this paper.

From Figures 9–12, we can find that the standard fractional-order adaptive controller in [23], the fractional adaptive controller in [24] and our proposed adaptive controller all can make the tracking error bounded so that $x_p(t)$ follows $x_m(t)$. Moreover, from Figures 9 and 10, taking the 5% error band, we can obtain that the response adjustment times of e_1 and e_2 with the standard fractional-order adaptive controller, the fractional adaptive controller in [24] and our proposed adaptive controller are 3.1033 s, 2.9814 s, 7.5304 s, and 1.5791 s, 1.029 s, 3.5002 s, respectively. Moreover, the ratio of overshoot of e_1 and e_2 is 0.3152:0.1941:0, and 0.3063:0.1895:0, respectively. Therefore, compared with the other two fractional-order adaptive controllers, the response adjustment time of our controller is relatively longer, but the overshoot is smaller.

Based on the above analysis, our control architecture can reduce the online computation burden while maintaining the stability of the tracking error.

6. Conclusions and Discussion

For fractional-order multivariable systems with parameter uncertainty, as the inputoutput dimension of the FOMRAC system increases, the number of parameters that need to be updated online in the controller also increases, which will increase the computational cost and resource consumption for increasingly complex systems. Motivated by this, a FOMRAC scheme based on the nonlinear scalar update law has been designed in this paper to relieve the computational burden existing in fractional-order controllers and ensure that the desired tracking performance can be achieved. Specifically, the scalar update law does not change as the input–output dimension changes. Compared with the existing results, the main advantage of the proposed adaptive controller is that only one parameter online update is needed such that the control scheme is computationally inexpensive. Moreover, we prove the boundedness of all signals involved in this adaptive scheme and the convergence to zero of the mean value of the squared norm of the error. Two illustrative numerical examples are presented to confirm the efficiency of the proposed architecture. As for future perspectives, our research efforts will generalize our work to nonlinear fractional-order systems, input–output multivariable fractional-order systems and fractional-order systems with limited state information.

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