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# Bifunctional TiO<sub>2</sub>/AlZr Thin Films on Steel Substrate Combining Corrosion Resistance and Photocatalytic Properties

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**Abstract:** A novel multi-functional bilayer coating combining an anti-corrosion Al–Zr (4 at.% Zr) underlayer and an anti-biofouling TiO<sub>2</sub> top layer was deposited on high-speed steel (HSS) substrates. Al–Zr (4 at.% Zr) film, deposited by DC magnetron sputtering, which is a single phased supersaturated solid solution of Zr in Al, is used to provide sacrificial corrosion resistance of steels and TiO<sub>2</sub> is added as a top layer to induce photocatalytic activity and hydrophilic behavior which can generate antifouling properties in order to slow down the biofouling process. The top TiO<sub>2</sub> films, deposited at 550 °C by AACVD (aerosol-assisted chemical vapor deposition), consisting of anatase TiO<sub>2</sub> microflowers physically attached to the TiO<sub>2</sub> thin films present a high decomposition rate of Orange G dye ( $780 \times 10^{-10} \text{ mol L}^{-1} \cdot \text{min}^{-1}$ ). The enhanced photocatalytic performance is associated with the rough network and the presence of TiO<sub>2</sub> microflowers capable of supporting the enhanced loading of organic contaminants onto the film surface. Electrochemical tests in saline solution have revealed that bilayer films provide cathodic protection for the steel substrate. The Al–Zr/TiO<sub>2</sub> bilayer presents a lower corrosion current density of  $4.01 \times 10^{-7} \text{ A/cm}^2$  and a corrosion potential of  $-0.61 \text{ V}$  vs. Ag/AgCl, offering good protection through the preferential oxidation of the bilayer and an increased pitting resistance. The proposed functionalized coating combining anticorrosion and photocatalytic properties is a promising candidate for an anti-fouling system in sea water.

**Keywords:** Al–Zr; TiO<sub>2</sub>; corrosion; photocatalysis; aerosol CVD; magnetron sputtering

## 1. Introduction

Marine biofouling is the growth and accumulation of micro and macro-organisms on wet surfaces in saline environments and it is a global problem disturbing aquatic industries. Biofouling can reduce the speed of ships, boost fuel consumption, and stimulate corrosion, which provokes mechanical deterioration of static structures [1]. Biofouling takes place on almost all surfaces starting with the attachment of organic molecules pursued by adherence of bacteria, diatoms, and microalgae to create a biofilm that is followed by the adhesion of macro-organisms, such as barnacles, bivalves, and macro-algae [2,3]. Priyanka et al. [4] have demonstrated that photocatalytic material can prevent

biofouling by generating reactive oxygen species under visible light irradiation, which in a marine environment can lead to cell death in a variety of contaminants [5–7].

The corrosion of metals in natural seawater is a consequence of interactions between metal, living organisms, and seawater composition [8]. When a metal is submerged into seawater, corrosion, and biofouling take place on almost the same time proportions [9]. This is usually pursued by the development of biofilm within days after submersion [10] and after a continued exposure, macrobiota like invertebrate larvae may combine with the biofilm and settle on the surface [11].

To solve this problem, we address two functional properties: photocatalysis, which is related to the surface properties to avoid the initial step of attachment, and corrosion, to protect the steel used in the mechanical system. Cathodic protection systems might be able to polarize all underwater steel structures to a potential between  $-800$  and  $-1100$  mV vs. the Ag/AgCl/seawater reference electrode, and to preserve the potential in this interval throughout the life of the structures [12].

Titanium is the most abundant transition metal on earth and its metal oxide  $\text{TiO}_2$  is a wide band-gap semiconductor with high chemical stability, low-cost, non-toxicity, and high photoelectric conversion productivity. In recent years, titanium dioxide ( $\text{TiO}_2$ ) has been extensively investigated for its remarkable UV-photocatalytic and self-cleaning properties, which, for example, can promote the decomposition of organics present into harmless products under UV light irradiation [13]. The extent of the photo-activity depends on an extensive variety of properties, such as morphology, crystallinity, and surface area.

$\text{TiO}_2$  possesses unique electronic properties combined with the possibility of easy nanostructuring and chemical stability. Typically, when the surface of a semiconductor material is exposed to photons having energy greater than or equal to its band-gap energy, photo-electrons  $e^-$ , and photo-holes  $h^+$  are produced [14]. As the photocatalyst is simultaneously capable of adsorbing reactants and absorbing photons, the photogenerated  $e^-$  and  $h^+$  are thus capable of reducing and oxidizing pollutants adsorbed on the photocatalyst's surface [15].

Nano and microstructures play an important role in enhancing the performance of devices, mainly due to the increase of the specific surface area [16] as for photocatalyzed reactions.  $\text{TiO}_2$  structures that have a high mesoporosity and surface area are mostly attractive, as these increase the efficiency of photocatalysis phenomena taking place at the interfaces. Morphology, structure, phase, and dimensionality adjust physical and chemical properties of the  $\text{TiO}_2$  nanostructures. Tian [16] demonstrated that 3D flower-like  $\text{TiO}_2$  showed the highest UV light absorption when integrated in dye-sensitized solar cells (DSSC) compared to nanospheres and nanorod structures; even the photocatalytic activity (97% degradation efficiency) for flowers was higher than for spheres or rod-like structures (60% and 55%, respectively). These are mainly due to the fact that 3D hierarchical flower-like structures are easily accessible to light and reactants thanks to an increased effective surface area.

Zhu et al. [17] also demonstrated that anatase  $\text{TiO}_2$  materials having flowerlike morphologies with a high specific surface area presented an excellent performance when tested in photodegradation of methylene blue.

Aerosol assisted metal–organic chemical vapor deposition (AA-MOCVD) has been already demonstrated to deposit  $\text{TiO}_2$  films having hierarchical  $\text{TiO}_2$  microflowers. Biswas et al. [18] showed that AA-MOCVD working at atmospheric pressure allows the synthesis of  $\text{TiO}_2$  microflowers physically adhered to a thin film of  $\text{TiO}_2$ . We propose using these microstructures as a  $\text{TiO}_2$  active layer in the bilayer coating.

Aluminum and its alloys are extensively used in many industrial applications as long as their open circuit potential is more negative than that of steel implying its use as sacrificial materials for the protection of steel. Aluminum-based alloy coatings have been extensively studied and proposed as potential candidates for galvanic corrosion protection of mechanical steel parts [19–25]. For instance, transition metals (TM) can be added to mechanically reinforce aluminum. The low solubility of TM in aluminum allows the deposition of extended supersaturated solid solution of TM in aluminum. Moreover, a good thermal stability due to the low diffusivity of TM in aluminum is expected. Addition of

high content of TM conducts typically to high mechanical properties compared to pure aluminum but with the detriment of sacrificial properties [26,27]. The ideal solution in terms of protection of steels agrees to a compromise between mechanical and corrosion properties.

Zirconium is a transition metal, which is known as a great grain refiner in traditional aluminum alloys [28]. It boosts mechanical properties [28] and improves considerably the corrosion resistance in deaerated borate-boric acid solution containing  $\text{Cl}^-$  [29]. Different to traditional methods where the Zr solid solubility is very low, non-equilibrium processing methods like rapid solidification [30], mechanical alloying [31], and sputtering technique [29,32,33] offer the possibility to achieve a supersaturated single solid solution with high Zr contents. In order to improve the efficiency of aluminum anodes, they are typically alloyed with other elements to encourage depassivation (breakdown of the oxide film) and/or shift the operating potential of the metal towards a more negative direction. Addition of alloying elements like Zr is characterized by an increase of the corrosion potential. Moreover, in the same time, increasing Zr content in Al allows one to lower the corrosion current density, which is associated with better corrosion resistance [34]. Al–Zr with 4 at.% Zr appears as the best compromise between the good corrosion behavior and the sacrificial character of the coating.

In this work, we propose a bilayer film consisting of a sputtered deposited crystalline Al–Zr film containing 4 at.% of Zirconium with a thickness of about 3  $\mu\text{m}$  as a sacrificial anode coating, and a  $\text{TiO}_2$  film deposited by the Aerosol CVD technique responsible for enhanced photocatalytic properties. The proposed functionalized coating is a promising candidate for an anti-fouling system in sea water.

## 2. Materials and Methods

### 2.1. Synthesis and Deposition Process

High speed steel (HSS) substrates with 30 mm in diameter and 1 mm thick were polished having a roughness average  $R_a$  equal to 47 nm. Substrates were degreased, rinsed with ethanol, and dried before the deposition. Aluminum–Zirconium alloy films (2.7  $\mu\text{m}$  thick) were co-deposited using standard DC magnetron sputtering (3-kW-SAIREM pulsed DC supply, equipped with a fast arc detector able to cut off micro-arcs within 1–2  $\mu\text{s}$ , Dephis, Etupes, France) of pure metallic Al and Zr targets at floating temperature. The unheated substrates (the floating temperature is below 70  $^\circ\text{C}$ ) were fixed on a rotating substrate-holder, at floating potential, ensuring a good homogeneity in thickness and composition of coatings. The sputtering chamber was pumped down via a mechanical pump and a turbo-molecular pump permitting a base vacuum of  $5 \times 10^{-4}$  Pa. The substrates surfaces were cleaned by an argon plasma etching at 200 W for 30 min to remove impurities, surface oxides and contaminates just before the deposition. The distance between targets and substrate-holder (8 cm), the argon flow rate (20 sccm) and the working pressure ( $P_{\text{Ar}} = 0.32$  Pa) were kept constant. Constant Zr content was ensured by fixing the Aluminum discharge current at 2 A and zirconium discharge current at 0.22 A. With these conditions, the deposition rate is about 1  $\mu\text{m}/\text{h}$  and the alloy composition is 4 at.% Zr. This composition led to the best compromise between intrinsic corrosion resistance, sacrificial character/steels, and mechanical reinforcement. Increasing Zr content in Al leads to a decrease in the mean grain size, which enhance its hardness. At the same time, the intrinsic corrosion resistance of these Al–Zr alloys is higher. However, above 4 at.% or 5 at.% of Zr in Al, these alloys become nobler than the steel substrate and the sacrificial character is lost [34].

$\text{TiO}_2$  films deposition were performed by AA-MOCVD (aerosol-assisted metal organic chemical vapor deposition) using a custom-designed and home-made reactor working at atmospheric pressure [35]. Titanium (IV) oxide bisacetylacetonate ( $\text{C}_{10}\text{H}_{14}\text{O}_5\text{Ti}$ , Strem Chemicals, Newburyport, MA, USA) was used as precursor and ethanol as solvent. The precursor was selected for its low-toxicity, good stability at room temperature, easy handling, and low cost. The titanium precursor was dissolved in ethanol with a concentration of 0.03  $\text{mol L}^{-1}$ . The aerosol was generated by a piezoelectric ceramic by adjusting the frequency and power (800 kHz, 60 W), forming a mist on top of the precursor solution. This mist was transported by air flow into the deposition chamber. An oxidizing gas flow was mixed

to the precursor flow consisting in  $6 \text{ L min}^{-1}$  of air (12% of  $\text{O}_2$ ). Within these conditions, the solution consumption was around  $3 \text{ mL min}^{-1}$ . A solution consumption between 3 and  $4 \text{ mL min}^{-1}$  allows the formation of hierarchical microflowers. However, less than  $3 \text{ mL min}^{-1}$  microflowers are not developed. The deposition temperature was varied between 500 and  $550^\circ\text{C}$  for a deposition time of 40 min. The substrates used in this work were high-speed steel or Al–Zr coated high-speed steel.

## 2.2. Characterization

### 2.2.1. Film Morphology, Surface Topography, and Thickness

Film morphology was observed by scanning electron microscopy (SEM) and composition by EDS microanalysis using an FEI Quanta 250 field-emission scanning electron microscope (FESEM, Hillsboro, OR, USA) for high-resolution images. Surface roughness profiles of samples were characterized using a Form Talysurf 50 (Taylor Hobson Co Ltd., Leicester, UK) surface Profilometer and measured 25 mm crossing the center along the surface of the sample. For these measurements, the pre-scan length used was 0.30 mm, the spacing ( $y$ ) was 0.1 mm, the measuring speed was 1 mm/s and the number of points was 5000. As described in ASME B46.1,  $R_a$  is the arithmetic average of the absolute values of the profile height deviations from the mean line, recorded within the evaluation length.  $R_a$  is the average of a set of individual measurements of the peaks and troughs of a given surface [36]. Thicknesses, which are evaluated from bright field images by TEM (JEOL JEM-2100F, Tokyo, Japan), are  $2.7 \mu\text{m}$  and  $1.4 \mu\text{m}$  for Al–Zr and  $\text{TiO}_2$ , respectively.

### 2.2.2. Structural Characterization

The crystallinity and phase identification of the samples were studied by X-ray diffraction (XRD) in  $\theta$ – $2\theta$  scanning mode using a Bragg–Brentano configuration between  $10^\circ$  and  $80^\circ$  at  $0.011^\circ$  intervals with an acquisition time of 2 s, using a Bruker D8 Advance diffractometer (Billerica, MA, USA) with monochromatic  $\text{Cu K}\alpha 1$  radiation ( $\lambda = 0.15406 \text{ nm}$ ).

The crystallite size was determined using the Scherrer's formula based on the FWHM (full width at half maximum) of (101), (200), and (211) anatase peaks in XRD patterns:

$$D_p = (K \times \lambda) / (\beta \times \cos\theta) \quad (1)$$

where  $D$  is the crystallite size in nanometers,  $\lambda_{\text{Cu}} = 0.15418 \text{ nm}$  is the X-ray wavelength,  $\theta$  is the diffraction angle of the (101), (200), and (211) peaks and  $\beta$  is defined as the peak width of the diffraction peak profile at half maximum height resulting from small crystallite size in radians and  $K$  is a constant related to crystallite shape. A value of 0.9 was assigned to the Scherrer's constant  $K$ .

Raman spectra were collected using a Jobin-Yvon/Horiba LabRam multichannel spectrometer (Kyoto, Japan) equipped with a liquid  $\text{N}_2$  cooled CCD detector. Experiments were conducted in the micro-Raman mode at room temperature in a backscattering geometry. The  $514.5 \text{ nm}$  line of an  $\text{Ar}^+$  laser ( $2.6 \text{ mW}$ ) was focused giving a spot size of about  $1 \mu\text{m}$ . The recorded spectra were calibrated using Si spectra at room temperatures. The integration times were adjusted in order to have a high signal-to-noise ratio.

Transmission electron microscopy (TEM) images were collected using JEOL JEM-2100F with an accelerating voltage of 200 kV. The point resolution of the TEM is  $0.19 \text{ nm}$ . TEM specimens were prepared by breaking the coating surface layers using a diamond knife and putting the obtained fine particles onto TEM copper grids coated with holey carbon films.

### 2.2.3. Photocatalytic Characterization

The photocatalytic activity of  $\text{TiO}_2$  films was evaluated by measuring the decomposition rate of aqueous Orange G solutions ( $C = 5 \times 10^{-5} \text{ M}$ ) using a UV–VIS Perkin Elmer Lambda 35 (Waltham, MA, USA). Absorbance spectra were acquired using a wavelength range from 400 to  $600 \text{ nm}$ .

The photocatalytic performance of TiO<sub>2</sub>/Al–Zr bilayer films were carried out by degrading orange G aqueous solution under UV irradiation. The degradation reaction was carried out in a beaker positioned on a support allowing it to be held at 20 mm above the UV lamps. The whole is placed in an oven regulated in humidity (RH = 40%) and temperature ( $T = 20\text{ }^{\circ}\text{C}$ ) under the UV light of three UV lamps (Philips PLS 11 W) emitting at 365 nm, chosen because absorption of Orange G is negligible at this wavelength. The surface area of the sample exposed to irradiation was 7.06 cm<sup>2</sup> and the radiance was 5 mW/cm<sup>2</sup>. The volume of initial Orange G aqueous solution was 50 mL. In order to homogenize the solution and to maintain constant adsorption/desorption conditions during UV exposure, the solution is stirred constantly during irradiation via a magnetic bar and a magnetic stirrer set at 500 rpm.

For a better comparison, we analyzed the kinetic linear simulation of degradation of Orange G, following the pseudo-first-order kinetics model due to the low initial Orange G concentration. The equation is described as [37]:

$$r = -dC/dt = k_c(K_{ads}C/(1 + kC)) \quad (2)$$

where  $r$  is the degradation rate of the reactant (mol L<sup>−1</sup> h<sup>−1</sup>),  $C$  is the concentration of reactant (mol L<sup>−1</sup>),  $t$  is the irradiation time,  $k_c$  is the kinetic constant of the reaction, and  $K_{ads}$  is the adsorption constant of the reactant. When the initial concentration is very low, the equation can be simplified to an apparent first-order model [37]:

$$\ln(C_0/C) = k_c \cdot K_{ads} \cdot t = K_{app}t \quad (3)$$

where  $C_0$  is the concentration of Orange G after the adsorption–desorption equilibrium,  $K_{app}$  is the apparent first-order rate constant (h<sup>−1</sup>).

The constant  $k$  was used to compare the photocatalytic activities of the different samples.  $k$  describes an apparent kinetic constant of the system.

#### 2.2.4. Electrochemical Tests

The electrochemical measurements were carried out in an aerated and stirred chlorine solution (5 wt.% NaCl solution) using an Autolab potentiostat driven by NOVA 2.0 software (Metrohm Autolab, Utrecht, Netherlands). A total of 3 measurements were performed for each sample. The pH of the solution was adjusted to 6 by the addition of 0.5 M HCl solution and each measurement was performed at room temperature. The potentials were referenced against an Ag/AgCl electrode and the counter electrode was a large platinum grid. The effective area of working electrode was 1.327 cm<sup>2</sup>. The polarisation curves were recorded in the potential range of  $\pm 150$  mV around the open circuit potential (OCP) at a scan rate of 0.2 mV/s after 1 h of immersion in the saline solution. The corrosion potential  $E_{corr}$  and corrosion current density  $I_{corr}$  were estimated from the cross-over point of the two tangents drawn on a linear portion of anodic and cathodic polarization curves. The evolution of open circuit potential was recorded during 1 h.

#### 2.2.5. Coating Hydrophilicity

The hydrophilicity was evaluated by measuring the contact angle and surface energy of water droplets with a goniometer KRÜSS G10 (Hamburg, Germany). A droplet of distilled water with 0.5  $\mu\text{L}$  volume was placed on its surface and the first contact angle was measured immediately. The contact angle was measured before and after the incidence of light in the UV-C region used for the evaluation of photocatalytic activities. Each value was an average of 3 measurements on different areas of the sample surface.

### 3. Results and Discussion

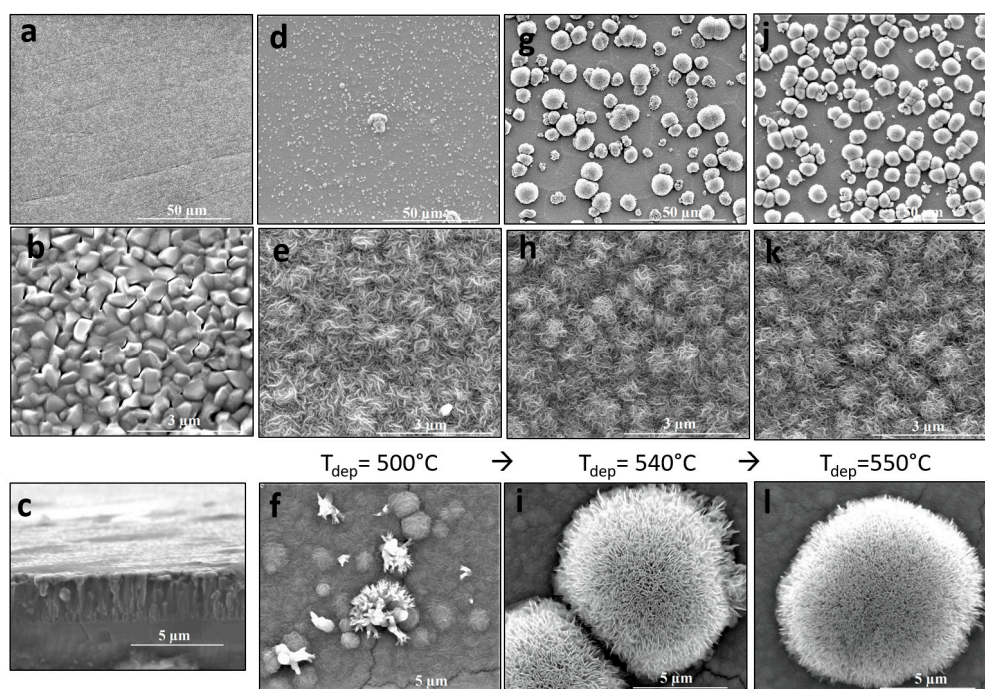
Polished high-speed steel (HSS) substrates were systematically covered with a previously optimized atomic composition Al–Zr coating [34]. Then, TiO<sub>2</sub> films were deposited at different



temperatures to determine the deposition conditions allowing the formation of flower-like microstructures, as described by Biswas et al. [18]. In this previous study, they proved that AACVD (aerosol-assisted chemical vapor deposition) allows the deposition of dense  $\text{TiO}_2$  layers containing hierarchical microflowers crystallized in the anatase phase and presenting a milky texture as a result of light scattering from the flowers. It was demonstrated that by adjusting the deposition conditions, it is possible to obtain  $\text{TiO}_2$  films containing  $\text{TiO}_2$  hierarchical microflowers on the surface [18]. Nevertheless, the formation of these hierarchical structures is obtained for a limited deposition condition window. These conditions are often reactor dependent and have to be tuned. To find the optimal deposition conditions, the solution concentration and solution feeding rate were fixed and deposition temperature varied between 500 and 550 °C. A feeding rate between 3 and 4 mL/min allows the formation of microflowers.

### 3.1. Morphology of Al–Zr and $\text{TiO}_2$ Films

The morphology of as-deposited Al–Zr films observed by SEM is shown in Figure 1a,b for low and high magnifications conditions in the upper and lower pictures, respectively, and in cross-section represented in Figure 1c. For low Zr contents like in our case and in our deposition conditions, the coatings grow with a columnar morphology forming big grains of around 500 nm of diameter. The Al–Zr coating thickness is 2.7  $\mu\text{m}$ . The hardness of this film is 2.3 GPa and Young's modulus  $E$  is 94.46 GPa. This material is susceptible to limit cracking from the top layer (Figure 1f) to the Al–Zr/steel interface. Nanoindentation experiment was impossible on the  $\text{TiO}_2$  top layer surface because of its particular morphology.



**Figure 1.** SEM images of samples: (a–c) Al–Zr (4 at.% Zr) coating, and  $\text{TiO}_2$  films deposited at (d–f) 500 °C, (g–i) 540 °C, and (j–l) 550 °C.

When  $\text{TiO}_2$  is deposited by AACVD as a second layer on the Al–Zr coating, two kinds of features appear. On one hand, a film consisting in small needle-like (dendritic microspheres) grains of 50 nm covered the Al–Zr grains in a very conformal way. This morphology can be observed in Figure 1e,h,k), for the three deposition temperatures used. The Al–Zr grains can be still identified even if  $\text{TiO}_2$  film thicknesses are around 1.4  $\mu\text{m}$ . On the other hand, microflowers started to grow for deposition temperatures higher than 500 °C. At 500 °C, represented in Figure 1d–f, some sparse flowers can be

observed but much smaller than those shown in Figure 1g–l) for films deposited at 540 and 550 °C, respectively. For films deposited at 540 and 550 °C, the flowers density increases. Flowers having an average diameter of about 7  $\mu\text{m}$  can be described by a homocentric association of  $\text{TiO}_2$  nanopetals forming a corolla as if growing from the receptacle of a flower. The main characteristics of these microstructure is that petals have a nanometric thickness ( $\sim 5$  nm) and are formed by nanocrystal of anatase phase as we show in the next section.

Figure 2 presents the surface roughness profiles for the HSS/Al–Zr sample and for the  $\text{TiO}_2$ /AlZr bilayer sample deposited at 500 and 550 °C.  $R_a$  values were measured using contact mode, where the measuring instrument was in direct contact with the surface.

Al–Zr monolayer film presents a rough surface with a  $R_a$  value of 87 nm. The roughness increases when  $\text{TiO}_2$  layer is added and also when the deposition temperature increases. The  $\text{TiO}_2$  film deposited at 500 °C, reproduces the Al–Zr baseline, with sparse peaks corresponding to the presence of microflowers. For  $\text{TiO}_2$  deposited at 540 °C, the density of microflowers is so high that provokes a very high roughness with an average  $R_a = 524$  nm. The highest variation in height corresponds to structures of 7  $\mu\text{m}$ , which are associated to the height of the biggest microflowers dispersed at the top of the layer.

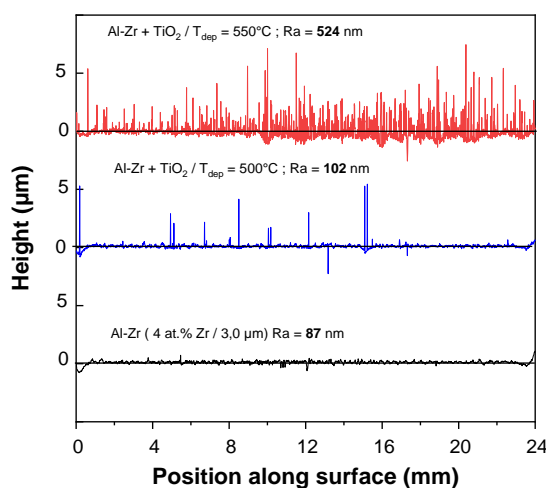


Figure 2. Surface roughness patterns measured 25 mm along the surface.

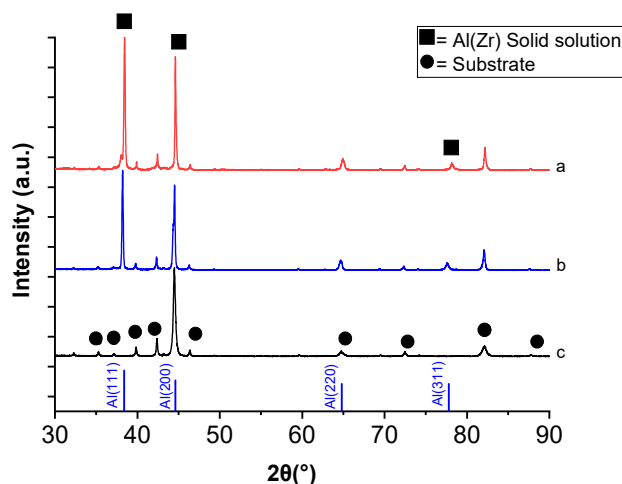
### 3.2. Structure Analysis

The structure of Al–Zr (4 at.% Zr) films was studied by XRD for the as deposited and also after annealing at 500 °C in air. The annealing was performed in order to check the Al–Zr stability during the  $\text{TiO}_2$  deposition by AACVD.

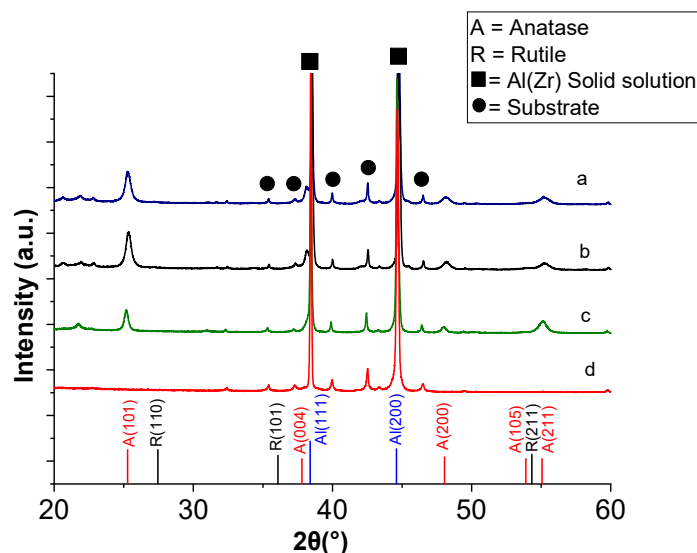
Figure 3 shows the XRD patterns for the HSS substrate together with the Al–Zr (4 at.% Zr) films deposited by DC magnetron sputtering in as-deposited conditions and after thermal annealing. HSS substrate is characterized by a large amount of Fe–Cr phase. The diffraction peaks in the diffractogram corresponding to as-deposited Al–Zr film can be correlated to an fcc structure indicating the growth of a supersaturated solid solution of Zr in Al without the presence of any parasitic phase.

When comparing the XRD patterns of Al–Zr film as deposited and annealed in air at 500 °C, no main changes are found; in both cases, the diffraction peaks of aluminum, with a very high intensity of (111) diffraction peak at 38° is obtained, suggesting the presence of  $\alpha$ -Al solid solution.

XRD characterisation was also performed after deposition of  $\text{TiO}_2$  at 500, 540 and 550 °C on the Al–Zr coated substrates for a deposition time of 40 min. The XRD patterns of these  $\text{TiO}_2$  coatings are shown in Figure 4. They reveal anatase phase in all samples, mainly detected by the (101) and (200) diffraction peaks at 25° and 48°, respectively, without the presence of a rutile phase, even for the highest deposition temperature of 550 °C. This is favorable because rutile has a lower charge-transfer rate and higher recombination rate of photogenerated electron–hole pairs than anatase [38].



**Figure 3.** XRD patterns for the (a) HSS substrate, (b) as-deposited Al–Zr film on high-speed steel substrate, and (c) Al–Zr film annealed in the air at 500 °C.

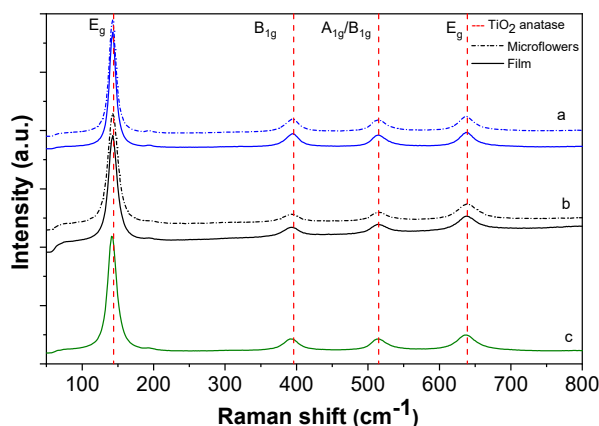


**Figure 4.** XRD patterns for TiO<sub>2</sub> films deposited at (a) 550 °C, (b) 540 °C, and (c) 500 °C on (d) Al–Zr.

Many works have been reported in the literature about the Raman signature of the different TiO<sub>2</sub> phases [39]. Moreover, this technique is more sensitive to anatase, rutile, and amorphous phases of TiO<sub>2</sub> films than XRD [40]. Besides, the technique is very local, allowing one to probe different microstructures at the sample surface.

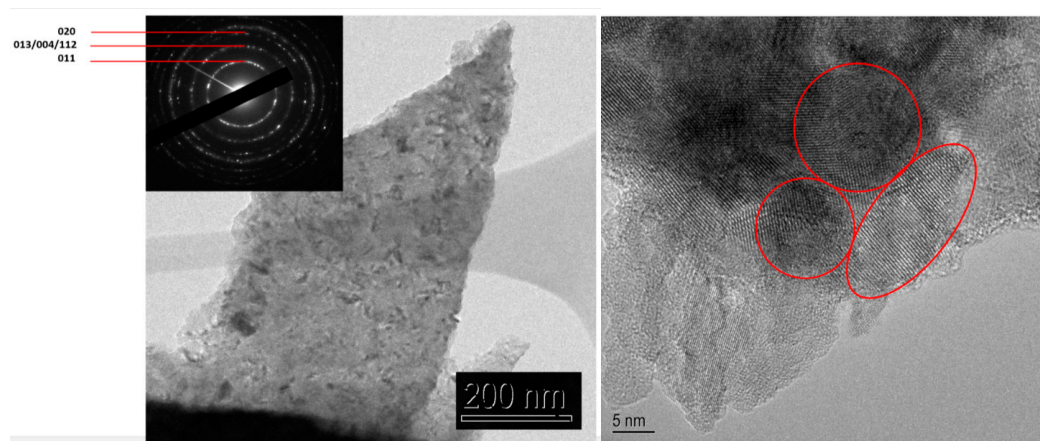
Figure 5 shows the Raman spectra of TiO<sub>2</sub>/Al–Zr multilayers for films deposited at different temperatures ranging between 500 and 550 °C. The Raman spectra of the film containing microflowers on the surface shows characteristic modes of the TiO<sub>2</sub> anatase phase [41]: two  $E_g$  modes at 141 and 635 cm<sup>−1</sup>, one  $A_{1g}$  mode at 513 cm<sup>−1</sup> and one  $B_{1g}$  mode at 397.5 cm<sup>−1</sup>. The sharp peak at 144 cm<sup>−1</sup> clearly identifies the anatase phase of TiO<sub>2</sub>. Smaller peaks at 398 and 639 cm<sup>−1</sup> can also be assigned to the anatase phase. No band corresponding to the rutile phase of TiO<sub>2</sub> was observed. Moreover, the absence of a broadband background in the Raman spectra allows one to discard the growth of amorphous TiO<sub>2</sub>.





**Figure 5.** Raman spectra for TiO<sub>2</sub> films deposited by aerosol CVD at (a) 550 °C, (b) 540 °C, and (c) 500 °C.

TEM observations show that the coatings are composed of anatase TiO<sub>2</sub> nanograins as deduced from the diffraction pattern (Figure 6) with a grain size about 10–20 nm.

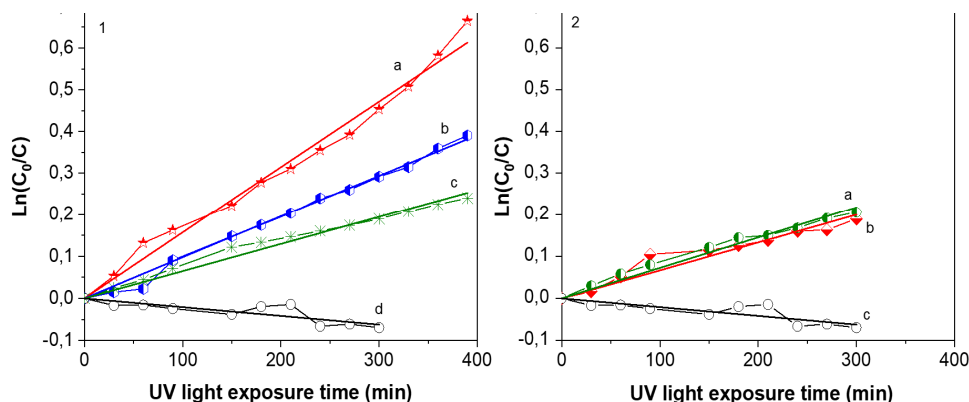


**Figure 6.** Bright field image from TiO<sub>2</sub>/Al-Zr film and the corresponding selected area electron diffraction pattern indicate the formation of the nanocrystalline anatase TiO<sub>2</sub> phase.

### 3.3. Photocatalytic Properties

The evolution of the absorption band at 480 nm corresponding to Orange G allows one to quantify the concentration variation with UV exposure time. Figure 7 shows plots of  $\ln(C/C_0)$  as a function of UV light irradiation time. Al-Zr coating was tested for verification and, as expected, this layer doesn't present any photocatalytic activity as indicated by an almost constant slope. On the contrary, the concentration of orange G decreases when exposed to TiO<sub>2</sub> films. Two kinds of TiO<sub>2</sub> films were deposited to highlight the influence of microflowers in photocatalytic properties. Using the same deposition temperature, the precursor flowrate was slightly decreased to deposit TiO<sub>2</sub> films without flowers. These layers present the same morphology and crystallized also in anatase phase (SEM and XRD are shown in the Supplementary Materials). The photocatalytic activity of these 2 series are represented in Figure 7. For films containing TiO<sub>2</sub> microflowers, the deposition temperature has an influence on the degradation rate, with a maximum value in the case of the film deposited at 550 °C, which shows 50% of mineralization after 400 min of UV light exposure. For the film deposited at 540 °C, the value is 30% of mineralization for the same exposition time and only 20% for the film deposited at 500 °C. It is important to notice that microflowers structure were mainly present in samples deposited at 540 and 550 °C, creating a higher roughness and a larger surface for chemical exchange or reaction. The  $k$  constant for Orange G degradation calculated from the slope with Formula (3) is resumed in Table 1. For films without microflowers deposited at 500 and 550 °C, as represented in Figure 7-2,

the  $k$  constant obtained by a linear regression is one order of magnitude lower than films containing microflowers deposited at the same temperature.



**Figure 7.** Evolution of the orange G degradation with UV light (371 nm) versus irradiation time for the TiO<sub>2</sub>/Al-Zr thin films deposited at (1a) 550°, (1b) 540 °C, (1c) 500 °C, with microflowers (left) and TiO<sub>2</sub>/Al-Zr thin films deposited at (2a) 500°, (2b) 550 °C without microflowers (right). The evolution of Al-Zr films are also presented on (1d) and (2c) for comparison.

**Table 1.** Constant  $k$  (kinetic constant of the system) for TiO<sub>2</sub>/Al-Zr coatings deposited at different temperatures.

Samples with Microflowers	Constant $k$ (min <sup>-1</sup> )
Al-Zr + TiO <sub>2</sub> $T_{\text{dep}} = 500$ °C	0.00063
Al-Zr + TiO <sub>2</sub> $T_{\text{dep}} = 540$ °C	0.00102
Al-Zr + TiO <sub>2</sub> $T_{\text{dep}} = 550$ °C	0.00156
Samples without Microflowers	Constant $k$ (min <sup>-1</sup> )
Al-Zr + TiO <sub>2</sub> $T_{\text{dep}} = 500$ °C	0.00066
Al-Zr + TiO <sub>2</sub> $T_{\text{dep}} = 550$ °C	0.00059

Eufinger et al. demonstrated that low grain diameter (<50 nm) increases the active surface area [42]. Other papers show that TiO<sub>2</sub> photoactivity is related to grain size [43]. In our case, films are formed of a double morphology that evolves in a different way. To determine the crystallite size evolution with temperature on the dense TiO<sub>2</sub> film without flowers, we performed XRD diffraction on TiO<sub>2</sub>/Al-Zr films deposited on polished HSS substrate. In this case, the grain size obtained by Scherer's method given in Formula (1) are 44 nm for film deposited at 500 °C and 53 nm for films deposited at 550 °C. However, if we calculate crystallite size from the samples containing flowers, the values are 18 nm and 20 nm for 500 and 550 °C, respectively. As the mean value includes the crystallites size from the film that should be equivalent to previous values in TiO<sub>2</sub> films, we can infer that crystallites size contained in the microflowers are rather smaller to 18 nm, in agreement with TEM observations. The crystal values for TiO<sub>2</sub>/Al-Zr coatings deposited at 500 and 550 °C are resumed in Table 2.

The decomposition rate (DR) is calculated by multiplying the initial concentration of Orange G  $C_0 = 5 \times 10^{-5}$  M by the constant  $k$ . These values are also resumed in Table 2 for the TiO<sub>2</sub>/Al-Zr coatings deposited at 500 and 550 °C.

Maury et al. [44] reported a maximum DR of Orange G solution (10 ppm) of about  $280 \times 10^{-10}$  mol L<sup>-1</sup> min<sup>-1</sup> for TiO<sub>2</sub> films deposited at 400 °C by AAMOCVD containing pure anatase phase.

In our work, the increase in decomposition rate from  $332 \times 10^{-10}$  mol L<sup>-1</sup> min<sup>-1</sup> for the TiO<sub>2</sub>/Al-Zr film deposited at 500 °C to  $780 \times 10^{-10}$  mol L<sup>-1</sup> min<sup>-1</sup> for the sample deposited at 550° is observed

only in samples containing flowers. For samples without flowers the DR is similar or even lower than reported values.

The presence of microflowers with nanometric crystallite size contributes to a large specific surface, which can enhance the photocatalytic activity and improves the degradation rate of organic pollutants by multiplying the active sites for absorption in  $\text{TiO}_2$  [45,46]. By increasing the surface area, adsorption of the reactants upon the photocatalyst and absorption of the light will increase. This is the twofold interest of the microflower activity.

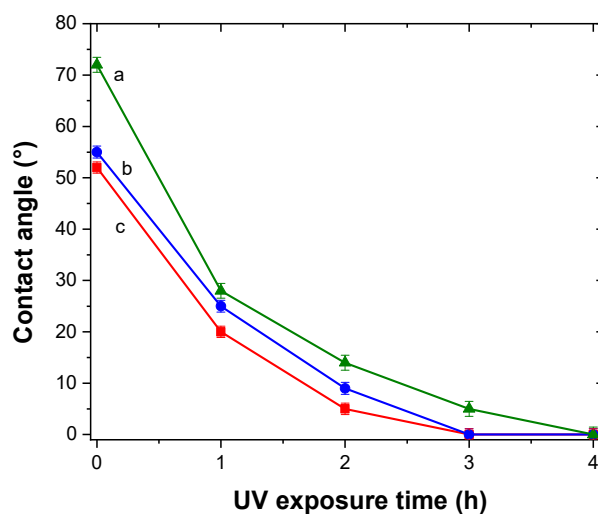
**Table 2.** The effect of presence of microflowers on the decomposition rate and the crystal size for the  $\text{TiO}_2/\text{Al-Zr}$  coatings deposited at 500 °C and 550 °C.

Samples with Microflowers	DR ( $10^{-10} \text{ mol L}^{-1} \text{ min}^{-1}$ )	Crystal Size (nm)
Al-Zr + $\text{TiO}_2$ $T_{\text{dep}} = 500 \text{ }^\circ\text{C}$	510	18
Al-Zr + $\text{TiO}_2$ $T_{\text{dep}} = 550 \text{ }^\circ\text{C}$	780	20
Samples without Microflowers	DR ( $10^{-10} \text{ mol L}^{-1} \text{ min}^{-1}$ )	Crystal Size (nm)
Al-Zr + $\text{TiO}_2$ $T_{\text{dep}} = 500 \text{ }^\circ\text{C}$	332	44
Al-Zr + $\text{TiO}_2$ $T_{\text{dep}} = 550 \text{ }^\circ\text{C}$	297	53

### 3.4. Hydrophilicity of $\text{TiO}_2/\text{Al-Zr}$ Bilayer Films

Hydrophilicity is usually present in materials with photocatalytic activity [46]. This property can be enhanced, and even restored, by UV exposure. The self-cleaning property is directly related to this material feature [46].  $\text{TiO}_2/\text{Al-Zr}$  thin films were irradiated with UV light during 4 h and the water contact angle was measured at different exposure times. A total of 10 measurements were made for each sample and results are presented in Figure 8. For all the samples, the contact angle decreases sharply with the time from values around 60° and reaching 0° after 4 h of UV exposure indicating a photoinduced superhydrophilicity. After six months in the absence of UV irradiation, the samples remained superhydrophilic presenting a contact angle of about 5°.

In the water contact angle measurements, high photoactivity means that the photogenerated holes attract hydroxyl groups from water and produce hydroxyl radicals ( $\bullet\text{OH}$ ). The higher the number of hydroxyl molecules on the surface, the higher is its hydrophilicity. This is presented as a small contact angle between the water droplet and the  $\text{TiO}_2$  surface.



**Figure 8.** Variation of water contact angles under UV illumination with time for  $\text{TiO}_2/\text{AlZr}$  bilayer samples deposited at (a) 500 °C, (b) 540 °C, and (c) 550 °C.

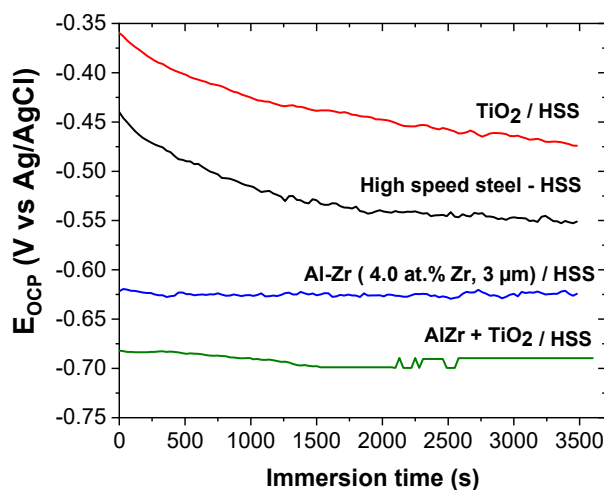
### 3.5. Electrochemical Behavior

Creus et al. presented the classification of aluminum based alloys in saline solution where the addition of Zr as a transition metal induces the ennoblement of the corrosion potential compared to pure aluminum without losing the sacrificial character [25]. In our work, Al–Zr films containing 4 at.% Zr were deposited on HSS substrate because this composition is the best compromise between mechanical properties, electrochemical behavior, and sacrificial character.

Figure 9 shows the evolution of the open circuit potential (OCP) versus time during 1 h of immersion in 5 wt.% NaCl for different coatings: Al–Zr,  $\text{TiO}_2$ , and the bilayer  $\text{TiO}_2/\text{Al–Zr}$ . The steel OCP is also reported as a reference. The steel OCP rapidly decreases and then stabilizes at around  $-0.55 \text{ V/Ag–AgCl}$ . This evolution is typical of the progressive formation of iron-based corrosion products on the steel surface [47]. The  $\text{TiO}_2$  coated steel presents a quite similar OCP evolution during the immersion suggesting that this evolution is directly linked to the steel degradation through the open defects of the oxide film. However, the OCP values are nobler in the presence of the titanium oxide layer. Ramaprakash et al. [48] also observed a slight ennoblement of the steel corrosion potential when is covered with  $\text{TiO}_2$  in 3.5% NaCl solution. This ennoblement was attributed to the modification of the electronic charge transfer during the steel dissolution due to the presence of the oxide film.

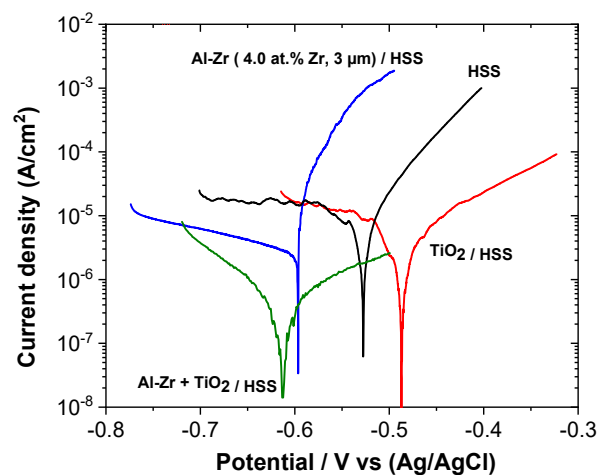
The OCP of the Al–Zr coating is quite constant during the immersion at around  $-0.62 \text{ V/Ag–AgCl}$ , which seems to be closed to the pitting potential as mentioned in [25] for similar Al-based coatings in saline solution. The OCP of the bilayer  $\text{TiO}_2/\text{Al–Zr}$  coating is also quite constant during the immersion at around at  $-0.69 \text{ V/Ag–AgCl}$ , which is slightly more negative compared with the Al–Zr coating. The shift of the OCP towards more negative values was also reported by Dias et al. on  $\text{TiO}_2$  thin films deposited by atomic layer deposition on Al–Mn alloys [49].

The OCP measurements prove that Al–Zr and  $\text{TiO}_2/\text{Al–Zr}$  bilayer coatings keep the sacrificial character. It seems that the presence of the  $\text{TiO}_2$  coatings acts differently when is deposited onto steel or aluminum based materials, this could be due to the intrinsic properties of the titanium oxide film.



**Figure 9.** Evolution of OCP potential of steel coated with Al–Zr (4 at.% Zr) film and  $\text{TiO}_2/\text{Al–Zr}$  bilayer films vs. immersion time in 5 wt.% NaCl.

The polarization curves of the coated steels: Al–Zr,  $\text{TiO}_2$ , and the bilayer  $\text{TiO}_2/\text{Al–Zr}$  are presented in Figure 10 and compared with the bare steel. Corrosion potential ( $E_{\text{corr}}$ ) and corrosion current density ( $I_{\text{corr}}$ ) were determined from the polarization curves by imposing a straight line along the linear portion of the anodic and cathodic curve and extrapolate it through  $E_{\text{corr}}$ . Table 3 gathers the corrosion current density and corrosion potential values extracted from the potentiodynamic test for all the samples.



**Figure 10.** Polarisation curves of Al–Zr (4 at.% Zr), TiO<sub>2</sub>, and TiO<sub>2</sub>/Al–Zr bilayer films deposited on HSS after 1 h of immersion in 5 wt.% NaCl.

**Table 3.**  $I_{\text{corr}}$  and  $E_{\text{corr}}$  values for Al–Zr, TiO<sub>2</sub> films, Al–Zr/TiO<sub>2</sub> films, and HSS substrate.

Samples	$I_{\text{corr}}$ (A/cm <sup>2</sup> )	$E_{\text{corr}}$ (V/(Ag/AgCl))
HSS substrate	18 + −2	−0.52 + −0.05
TiO <sub>2</sub>	9 + −1	−0.48 + −0.05
Al–Zr (4 at.% Zr)	2.5 + −0.3	−0.59 + −0.06
Al–Zr + TiO <sub>2</sub>	0.41 + −0.05	−0.61 + −0.06

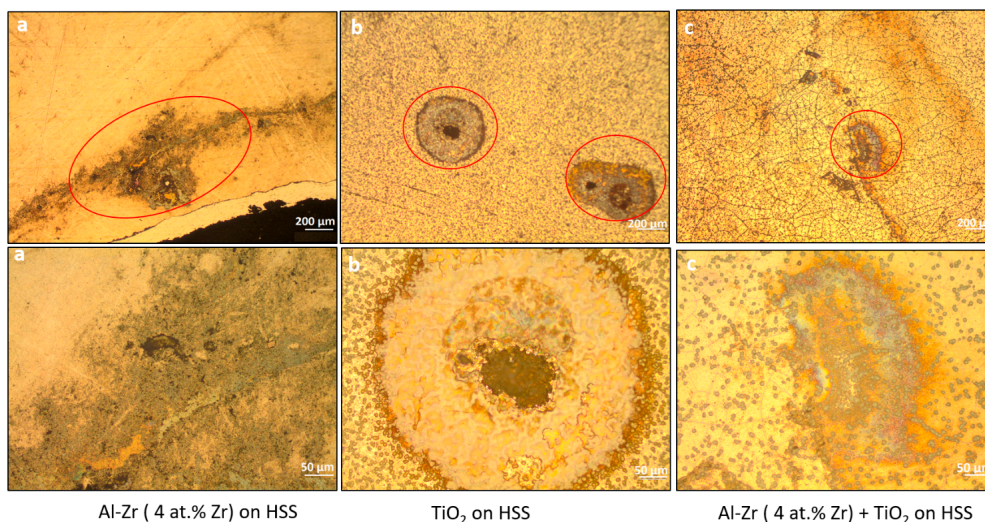
The corrosion potential of the bare steel after one hour of immersion in stirred saline solution is around −0.52 V vs. Ag/AgCl. A diffusional plateau is observed in the cathodic domain corresponding to the dioxygen reduction and a uniform corrosion is observed in the anodic domain. The TiO<sub>2</sub> film induces a shift of the corrosion potential towards more positive values as observed by Ramaprakash et al. [48]. The cathodic branch is not affected by the presence of the titanium oxide film, whereas the steel dissolution mechanism is modified. The anodic slope is decreased suggesting that the oxide film affects the charge transfer reactions during the steel dissolution.

Al–Zr coating presents a corrosion potential at around −0.59 V vs. Ag/AgCl which is slightly more negative compared to the HSS substrate suggesting that the Al-based coatings present a sacrificial behavior compared to steel. The anodic polarization curve presents a sudden rise in current close to the corrosion potential corresponding to the initiation of pitting corrosion as presented by Creus et al. [25]. We can notice that the initiation of the pitting corrosion occurs at a potential value that is close to the corrosion potential.

The polarization curve for the bilayer coated sample (TiO<sub>2</sub>/Al–Zr) is quite different from the other configurations. The influence of the TiO<sub>2</sub> film on the corrosion behavior is different when deposited on HSS steel or on Al–Zr coating, probably due to the fact that steel suffers from a uniform corrosion whereas pitting corrosion is the main degradation observed on Al–Zr coating. The TiO<sub>2</sub> oxide film affects the cathodic domain with an increase of the cathodic reaction slope associated with the dioxygen reduction, suggesting that the charge transfer step in the dioxygen reduction reaction is slow down. The TiO<sub>2</sub> film permits to reduce the contribution of the cathodic reactions leading to the decrease of the corrosion current density, down to  $4.1 \times 10^{-7}$  A/cm<sup>2</sup>. As observed for the Al–Zr coating, the pitting corrosion occurs at potential values very close to the corrosion potential, but in the bilayer coating, we can suppose that the pit initiation is mainly localized near the oxide film defects. An important decrease of the anodic reaction kinetic probably due to the increase of the surface impedance associated to the TiO<sub>2</sub> layer is observed. So the pit propagation seems to be reduced in the presence of the oxide film.



The optical observations of the corroded surface of the coated samples after the potentiodynamic polarization are presented in Figure 11. It shows that the mean pit diameter decreases when  $\text{TiO}_2$  is added as a second layer. It suggests that the  $\text{TiO}_2$  coating impede the growth of pits. We can infer that the  $\text{TiO}_2$  layer is able to increase the pitting resistance due to the fact that the cathodic reaction kinetic is lower.



**Figure 11.** Optical micrographs of pits formed on (a) Al-Zr (4 at.% Zr), (b)  $\text{TiO}_2$ , and (c)  $\text{TiO}_2/\text{Al-Zr}$  bilayer films deposited on HSS after 1h of immersion in 5 wt.% NaCl.

#### 4. Conclusions

The potential functionality of a  $\text{TiO}_2/\text{Al-Zr}$  bilayer coating combining anticorrosion and photocatalysis properties has been tested using high-speed steel (HSS) as substrates. The Al-Zr thin films containing a supersaturated solid solution with 4 at.% Zr were deposited on HSS substrates by DC magnetron sputtering. Then,  $\text{TiO}_2$  coatings were deposited by aerosol-assisted CVD in optimized conditions to grow a microstructure characterized by the presence of  $\text{TiO}_2$  microflowers physically attached to the  $\text{TiO}_2$  thin film. Optimal growth conditions were obtained by the combination of deposition temperature, precursor concentration, and precursor feeding rate [18]. XRD and Raman spectroscopy confirm that  $\text{TiO}_2$  microflowers and thin film consist of  $\text{TiO}_2$  in anatase phase. The presence of  $\text{TiO}_2$  microflowers having a diameter and height of about  $7\ \mu\text{m}$  and a crystallite size of 20 nm plays a crucial role in photocatalysis of Orange G compound. This behavior is enhanced on  $\text{TiO}_2$  samples deposited at  $550\ ^\circ\text{C}$ , showing a higher decomposition rate of Orange G ( $780 \times 10^{-10}\ \text{mol L}^{-1}$ ) under UV light irradiation when compared to others films deposited at lower deposition temperatures ( $500$  and  $540\ ^\circ\text{C}$ ).

Finally, Al-Zr/ $\text{TiO}_2$  bilayer coatings were found to be an interesting alternative to preserve sacrificial character for the protection of steel structures in saline environments, showing a corrosion potential of  $-0.61\ \text{V}$  vs. Ag/AgCl.  $\text{TiO}_2/\text{Al-Zr}$  bilayer coatings deposited on steel substrates offer good protection through the preferential oxidation of the bilayer presenting a lower corrosion current density of  $4.01 \times 10^{-7}\ \text{A/cm}^2$ .  $\text{TiO}_2$  as a second layer reduces the electrochemical activity of the films through the formation of a dense passive film and also increases the pitting resistance since the cathodic reaction kinetic is lower.

This study confirms the fundamental role of roughness and superhydrophilicity on the photocatalysis process and encourage the application of  $\text{TiO}_2$  nano-coatings for the fabrication of components to avoid algal adhesion on underwater structures. Biofouling field tests should be carried out in order to evaluate the performance of coatings in real conditions.

**Supplementary Materials:** The following are available online at <http://www.mdpi.com/2079-6412/9/9/564/s1>, Figure S1: XRD Patterns for TiO<sub>2</sub>/Al-Zr thin films without microflowers deposited at (a) 500 °C, (b) 550 °C and (c) Al-Zr, Figure S2: XRD patterns for TiO<sub>2</sub>/Al-Zr thin films with microflowers deposited at (a) 550 °C, (b) 540 °C and (c) 500 °C on (d) Al-Zr, Figure S3: SEM images of TiO<sub>2</sub>/Al-Zr film without microflowers deposited at 550 °C, Figure S4: Decomposition of Orange G by TiO<sub>2</sub>/Al-Zr thin films with microflowers (left) deposited at (a) 550 °C, (b) 540 °C, (c) 500 °C and (d) Al-Zr as underlayer Zr under UV light (371 nm) irradiation time. TiO<sub>2</sub>/Al-Zr thin films without microflowers (right) deposited at (a) 500 °C and (b) 550 °C and (c) Al-Zr underlayer under UV light (371 nm) irradiation time.

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**Conflicts of Interest:** The authors declare no conflict of interest.

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